#### 6th symposium on pavement surface characteristics



#### DEVELOPMENT OF HALF-CAR BASED RUTTING INDEX

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### 1.1. Motivation



## Current approach: Rut Depth (RD) is...

- easy to obtain an individual value of the profile
- directly calculated from the measured profile





#### 1.2. Objective The new approach: based on the Human-Road-Vehicle Road-vehicle interaction Human (user) centered evaluation Long, Axis Development of $M_H, I_H$ Half-Car based index <sup>za</sup> Vehicle vibration $Z_1$ V(t) $\exists C_2$ User's ride sensation Trans. Axis $z_{p1}$ $z_{p2}$

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### 2. Mathematical Derivations



### Half-Car simulation model

$$\begin{split} M_2 \ddot{z}_1 &= K_2 (z_{p1} - z_1) - C_1 (\dot{z}_1 - \dot{z}_a) - K_1 (z_1 - z_a) \\ M_2 \ddot{z}_2 &= K_2 (z_{p2} - z_2) - C_1 (\dot{z}_2 - \dot{z}_b) - K_1 (z_2 - z_b) \\ M_H \ddot{z}_3 &= C_1 (\dot{z}_1 - \dot{z}_a) + K_1 (z_1 - z_a) \\ &\quad + C_1 (\dot{z}_2 - \dot{z}_b) + K_1 (z_2 - z_b) \\ I_H \ddot{\phi} &= \{C_1 (\dot{z}_1 - \dot{z}_a) + K_1 (z_1 - z_a)\} L \\ &\quad - \{C_1 (\dot{z}_2 - \dot{z}_b) + K_1 (z_2 - z_b)\} L \end{split}$$



 $I_H$ : roll moment of inertia,  $K_1$ : vehicle spring constant,  $K_2$ : tire stiffness, L: half of tread width,  $M_H$  spring mass,

 $M_2$ : unsprung mass,

 $z_a, z_b$ : sprung mass displacement,

 $z_{p1}, z_{p2}$ : transverse profile as inputs,

- $z_1, z_2$ : unsprung mass displacement,
- $z_3$ : vehicle cg. displacement,

 $\phi$ : roll rotation of sprung mass,

(cg. = center of gravity)

Parameter: Roll Rate



### 2. Mathematical Derivations Simulation Procedure The measurement data for input to the simulation is given as a single cross-section profile The simulation process requires successive crosssections toward forward direction Transition Speed enables the simulation for a single profile, and simulate lane-change maneuver $v(t) = V(t) * W_1 / \sqrt{W_1^2 + W_2^2}$ Primary Lane $W_{1}$ Secondary Lane $l = L * W_1 / \sqrt{W_1^2 + W_2^2}$ $W_{2}$ Definition of the transition speed





### Input Profile Data

- The input data is expanded by the combination with symmetrical itself
- First First
- The profile is assumed to have a constant slope between sampled elevation points







### Specifications of the Half-Car

### The set of specific parameter values that is often called Golden Car (by ASTM No. E1170)

$$K_1/M_H = 32(s^{-2}); K_2/M_H = 326(s^{-2}); M_2/M_H = 0.075;$$

 $C_1/M_H = 3(s^{-2}); I_H/(M_Hb^2) = 0.42; b = 2 * L = 1.8(m);$ 







## Driving Condition

The transition width W<sub>1</sub> and distance W<sub>2</sub> are decided on the basis of ISO 3888-1

 $W_1 = 3.5(m); \quad W_2 = 30(m)$ 

The simulated forward speed, V(t), is defined as 80km/h, then transition speed v(t) and I are

$$v(t) = 2.58(m/s); \quad l = 0.89(m)$$







### Definition of HRD

HRD: Half-Car based index for Rutting Distress

- The HRD is the root mean square (RMS) value of the roll rate from the Half-Car simulation
- Free HRD has unit of angular velocity such as rad/s

 $HRD = AVx_{RMS}$ 

where AVx<sub>RMS</sub>: RMS of roll rate of sprung mass (rad/s)





# Stationary HRD

For pavement monitoring applications, the HRD can be reported as a summarized value in some longitudinal segments





### 4. Applicability



- Which is the best estimator of rideability
  - Rut Depth is geometrically and directly calculated form the measured profile
  - HRD is computed from the measured profile based on the vehicle vibration response



- Subjective survey by a driving simulator
  - Comparison between Rut Depth and HRD
  - Applicability of HRD for the rutting evaluation



### 4.1. Driving Simulator



# **& KITDS**:

### Kitami Institute of Technology Driving Simulator

#### **Conventional simulator**

Safety of subjects
Easy setting of test conditions

Repeatability of test conditions

Economical testing

**KITDS** 

#### Road surface evaluation

- Roughness
- Rutting
- Skid resistance







### 4.2. Road Surface Characteristics 1 2 3 4 5

### Four rutted profiles were obtained form the PIARC EVEN data

#### Characteristics of the rutted profiles

Section	SITE in EVEN Project	Wearing/Flowing	Dual/Single
А	SITE3, Long. Dist.=220m	Flowing	Dual
В	SITE4, Long. Dist.=160m	Flowing	Single
С	SITE7, Long. Dist.=160m	Wearing	Single
D	SITE11, Long. Dist.=240m	Wearing	Dual





## 4.2. Road Surface Characteristics 1 2 3 4 5

### Evaluation Result of Analyzed Profiles

#### Calculation results of the indices

Section	Location	HRD:	Rut Depth - Average	Rut Depth - Peak
	in the EVEN Project	x 10 <sup>2</sup> rad/s	Method: mm	Method: mm
Α	SITE3, Dist.=220m	15.5	24	25
В	SITE4, Dist.=160m	5.5	14	25
С	SITE7, Dist.=160m	4.4	25	25
D	SITE11, Dist.=240m	6.3	25	25
Perfect	_	0	0	0
Smooth	-	0	0	0

Lane Line

Lane Line





#### 4.3. Driving Scenario



- 8 drivers were required to drive at one time on each analyzed profile
  - Double lane-change maneuver defined by the ISO
  - Keeping a constant driving speed of 60km/h





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#### 5. Conclusions



- This study developed a new index of rutting based on the vehicle vibration response
  - The HRD can be suitable for predicting the severity levels of rutting distress in terms of the drive's perception of ride quality.
  - Any definitions of rut depth cannot be applicable in the case of which profiles are indicated to the same depth with including the irregularities in their shapes



#### Thank you for your kind attention !!

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